



AD A O 42543

ODC FILE COPY



Evaluation of IR Countermeasures

OH-58 (Scout) Model Report (U)

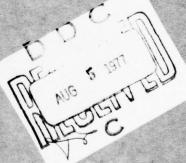
October 16, 1973

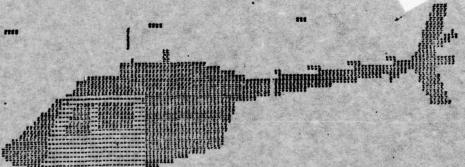
Prepared for

Program Manager
U.S. Army Aviation Systems Command
AMCPM-AEWSPS
Box 209, 12th and Spruce Street
St. Louis, Mo. 63166
Under Contract DAAJO1-72-0447, Exhibit A, Data A003

by

Westinghouse Electric Corporation Systems Development Division Strike Systems Avionics, M/S-434, Box 746, Baltimore, Md. 21203





Approved for public release;
Distribution Unlimited



Evaluation of IR Countermeasures

OH-58 (Scout) Model Report (U)

16 October 16, 1973

Prepared for

Program Manager
U.S. Army Aviation Systems Command
AMCPM-AEWSPS
Box 209, 12th and Spruce Street
St. Louis, Mo. 63166
Under Contract DAAJO1-72-0447, Exhibit A, Data A003

(15) DAAJOL-72-C-0447

Westinghouse Electric Corporation
Systems Development Division
Strike Systems Avionics, M/S-434
Box 746, Baltimore, Md. 21203

ACCESSIN for
NIS VINNE Section CON OUNANIOUNCED UNANIOUNCED UNANIO



This page intentionally left tlank.



#### Table of Contents

	Pa	ge
1.0	Introduction	-1
2.0	Helicopter Body Data	-1
3.0	Helicopter Operating Characteristics and Turbine Data	-1
3.1	Helicopter Operating Characteristics	-1
3.2	Turbine Data	-1
4.0	OH-58 Signature	-1
4.1	Input Data	-1
4.2	LOG Plot Signature	-4
4.3	Spectral Plot 4	<b>-</b> 6
4.4	Body Intercept Plot 4	-8
4.5	Grey Scale Plot	-8
4.6	Grey Shade Plot	-10
4.7	Grey Shade Photo	-10
Appe	ndix A Block Data of Body in the HIDE Mode	-1
Apper	ndix B Turbine Model for OH-58 Helicopter Be	-1
Appe	ndix C Selected Data from the OH-58 Operator's Manual	-1
Appe	ndix D Selected Data from Allison on the T63-A-700 Turbine D.	-1



## List of Figures

		Page
fron	atispiece OH-58 Scout	vi
2-1	OH-58 Surface Location	2-10
2-2	OH-58 Printout @ 70° Aspect with 20° Left Roll	2-1
2-3	OH-58 Silhouette Comparisons	2-13
4-1	Log Plot Signature	4-5
4-2	Spectral Plot	4-7
4-3	Body Intercept Plot	4-9
4-4	Grey Scale Plot	4-1
4-5	Grey Shade Plot	4-12
<b>4-</b> 6	Grey Shade Photo	4-12
	List of Tables	
	LISC OI TADIES	Page
2-1	OH-58 Helicopter Geometrical Structure Data	2-2
3-1	OH-58 Helicopter Speed and Torque Data for Cruise Speed	3 <b>-</b> 3
3-2	OH-58 Helicopter Speed and Torque Data for Maximum Cruise Speed	3-4
3-3	OH-58 Helicopter Speed and Torque Data for Hover	3-5
3-4	Engine Parameters at Standard Ambient Temperature	<b>3-</b> 6
3-5	Referred Power Turbine Outlet Total Temperature Versus Referred	
	Shaft Horsepower	3-7
3-6	Ambient Temperature Correction Factors	3-7



### List of Tables (Cont.)

														Page
4-1	Input Data		•	•			•		•					4-3
4-2	Spectral Priorities													4-8



Figure 1-1. OH-58A helicopter

RHD-10

OH-58 (Scout)



#### 1.0 (U) INTRODUCTION

The HIDE model is a comprehensive computer program designed to simulate the infrared signatures of Army aircraft.

The HIDE model was developed under contract DAA-J01-72-C-0447, "Evaluation of IR Countermeasures", for the U.S. Army Aviation Systems Command, AMCPM-AEWSPS. This work has been reported in two volumes:

Interim Technical Report (Model Methodology) 6-26-72 Final Technical Report (Phase II HIDE Model) 2-28-73

The original work developed the signature of a UH-1H helicopter. The work reported her is an extention to this contract to model an OH-58 helicopter to run in the HIDE model.

Section 2 defines the structural modeling referred to as body data. Section 3 describes the turbine and air frame operational models.

Section 4 presents a predicted signature after integration into the HIDE model.

Appendices are included which contain program elements and reference data.





#### 2.0 (U) HELICOPTER BODY DATA

The OH-58 body was dissected into eighty (80) surfaces as shown in Table 2-1. The technique used was that described in Appendix A of the Phase II Final Report. A breakdown of the helicopter by surface types shows:

#### 43 flats including:

17 rectangles (type 1).

3 discs (type 2),

23 trapesoids (type 3), and

37 conics including:

20 cylinders (type 4),

5 cones (type 5),

12 spheres (type 6), and

O circular parabolids (type 7).

An isometric drawing of the helicopter showing how the helicopter was dissected is presented in figure 2-1. A numbered baloon for each surface indicates surface number and type. Dashed baloons are used for surfaces on the right side of the helicopter which are mirror images of left side surfaces. In each case, the surface number for the right side surface is one higher than the surface number for the mirror image surface on the left side.

A large computer printout showing the helicopter at a 70° aspect angle off the nose is shown in figure 2-2.

The numbers on the helicopter represent the surface number. Certain areas such as the windows, rotors, and horizontal stabilizer are outlined for clarity. In figure 2-3, the front, top and side views from a computer

Evaluation of Countermeasures, Phase II HIDE Model Final Technical Report by Westinghouse Electric Corporation, February 28, 1972 (Secret)



Table 2-1. OH-58 Helicopter Geometrical Structure Data

SURFA(		SURFACE TYPE	FLIGHT STATION	WATER-	BULKHE	AD ALPHA
1	L. SIDE FUSELAGE	TRAPESOID	-121.000	192.900	26.000	.000
	R. SIDE FUSELAGE	TRAPESOID	-121,000	192.900	-26.000	•000
3	L. UPPER SIDE FUSELAGE	CYLINDER	-59.200	65.000	19.000	7.000
	R. UPPER SIDE FUSELAGE	CYLINDER	-59,200	65.000	-19.000	7.000
	L. UPPER CORNER FUSELAGE	SPHERE	-59,200	65.000	19.000	7.000
6	R. UPPER CORNER FUSELAGE	SPHERE	-59.200	65.000	-19.000	7.000
	7 UPPER FRONT FUSELAGE	CYLINDER	-59.200	65.000	.000	7.000
8	B L. FRONT CORNER FUSELAGE	CYLINDER	-59.200	65.000	19.000	7.000
9	R. FRONT CORNER FUSELAGE	CYLINDER	-59,200	65.000	-19.000	7.000
10	NOSE	CYLINDER	-8.000	33.000	•000	7.000
1:	L. SIDE NOSE	SPHERE	-8.000	33.000	7.000	7.000
12	2 R. SIDE NOSE	SPHERE	-8.000	33.000	-7.000	7.000
13	L. FRONT NOSE WINDOW	SPHERE	-8,000	33.000	7.000	7.000
14	R. FRONT NOSE WINDOW	SPHERE	-8,000	33.000	-7.000	7.000
15	L. NOSE WINDOW	CONE	21.000	33.000	2.000	13.400
16	R. NOSE WINDOW	CONE	21.000	33.000	-2.000	13.400
17	7 L. NOSE	CONE	21,000	33.000	2.000	13.400
16	B R. NOSE	CONE	21,000	33.000	-2.000	13.400
19	L. REAR OF NOSE	SPHERE	-37.000	33.000	12.000	14.000
2	R. REAR OF NOSE	SPHERE	-37.000	33.000	-12.000	14.000
2	1 TOP OF NOSE	TRAPESOID	32.550	30.200	•000	•000
2:	2 BOTTOM OF NOSE	TRAPESOID	32.550	35.900	.000	•000
2	3 FRONT OF WINDSHIELD	TRAPESOID	16,440	17.720	•000	•000
. 2	4 L. CORNER OF WINDSHIELD	CYLINDER	16.440	10.720	•000	7.000
	5 R. CORNER OF WINDSHIELD	CYLINDER	16.440	10.720	•000	7.000
						,,,,,,

2-2



Table 2-1. OH-58 Helicopter Geometrical Structure Data (Cont'd)

SURFACE NUMBER	BETA-	BETA-	GAMMA- MIN	GAMMA- MAX	PSI	THETA	PHI
1	127.900	173.900	.001	25.800	.000	6000	-90.000
2	-173.900	-127.900	154.200	180.000	.000	6000	90.000
3	.000	63.000	.001	360.000	.000	-906000	•000
4	.000	63.000	.001	360.000	.000	-90.000	•000
5	.001	180.000	.001	360.000	.000	6000	•000
6	.001	180.000	.001	360.000	•000	•000	•000
7	-19.000	19.000	.001	360.000	.000	•000	90.000
8	•000	51.000	180.000	360.000	.000	1546200	•000
9	•000	51.000	180.000	360.000	.000	1544200	•000
10	-7.000	7.000	.001	360.000	•000	•000	90.000
11	.001	90.000	.001	180.000	90.000	6000	•000
12	.001	90.000	90.000	270.000	.000	6000	•000
13	90.000	180.000	.001	180.000	90.000	•000	.000
14	90.000	180.000	90.000	270.000	.000	<b>€000</b>	•000
15	29,400	58.800	180.000	360.000	-9.800	906000	. •000
16	29.400	58.800	180.000	360.000	9.800	-904000	•000
17	29.400	58.800	.001	180.000	-9.800	-904000	•000
18	29.400	58.800	.001	180.000	9.800	-904000	•000
19	.001	180.000	.001	360.000	.000	.000	•000
20	.001	180.000	.001	360.900	•000	6000	•000
21	-71.500	-41.700	170.890	189.110	-90.000	6000	-13.400
22	-71.500	-41.700	170.890	189.110	-90.000	.000	13.400
23	-88.900	-37.000	167.950	192.050	-90.000	•000	-36.500
24	38,250	90.900	.001	360.000	-12.050	-53.500	•000
25	38.250	90.900	.001	360.000	12.050	-53.500	•000

2-3



Table 2-1. OH-58 Helicopter Geometrical Structure Data (Cont'd)

SURFACE HELICOPTER PART NUMBER DESCRIPTION	SURFACE TYPE	FLIGHT	WATER-	BULKHEAD LINE	ALPHA
26 L. SIDE OF WINDSHIELD	TRAPESOID	-13.640	33.000	15.000	.000
27 R. SIDE OF WINDSHIELD	TRAPESOID	-13,640	33.000	-15.000	.000
28 BOTTOM OF FUSELAGE	RECTANGLE	-121.000	19.000	.000	.000
29 OVERHEAD WINDOWS	RECTANGLE	-59.200	72.000	.000	.000
30 FRONT TOP FUSELAGE	RECTANGLE	-59.200	72.010	•000	•000
31 TOP FUSELAGE	RECTANGLE	-121.000	72.000	•000	•000
32 L. FRONT DOOR WINDOW	TRAPEZOID	-86,280	110.750	26.010	.000
33 R. FRONT DOOR WINDOW	TRAPEZOID	-86,280	110.750	-26.010	•000
34 L. BACK DOOR WINDOW	RECTANGLE	-114.000	65.000	26.010	.000
35 R. BACK DOOR WINDOW	RECTANGLE	-114.000	65.000	-26,010	•000
36 REAR TOP FUSELAGE	TRAPEZOID	-200,600	79.500	•000	•000
37 L. REAR UPPER SIDE FUSE.	CYLINDER	-200,600	72.500	.000	7.000
38 R. REAR UPPER SIDE FUSE.	CYLINDER	-200.600	72.500	.000	7.000
39 L. MID SIDE FUSELAGE	TRAPEZOID	-468,500	98.800	-56.500	.000
40 R. MID SIDE FUSELAGE	TRAPEZOID	-468,500	98.800	56.500	•000
41 MID AFT BOTTOM FUSELAGE	TRAPEZOID	-230.500	45.450	.000	.000
42 L. AFT SIDE FUSELAGE	TRAPEZOID	-200.600	72.500	7.000	.000
43 R. AFT SIDE FUSELAGE	TRAPEZOID	-200,600	72.500	-7.000	•000
44 AFT BOTTOM FUSELAGE	TRAPEZOID	-229.550	140.300	•000	•000
45 TAIL BOOM	CONE	-475,600	105.400	•000	1.450
46 END TAIL BOOM	SPHERE	-377,660	93.550	•000	2.500
47 TAIL ROTOR DRIVE SHAFT	CYLINDER	-474,600	108.400	•000	•500
48 TAIL ROTOR HUB	CYLINDER	-352.180	96.180	.000	1.000
49 TAIL ROTOR	RECTANGLE	-352,180	96.180	10.400	.000
50 HORIZONTAL STABILIZER	RECTANGLE	-270,000	79.800	•000	.000

2-4



Table 2-1. OH-58 Helicopter Geometrical Structure Data (Cont'd)

SURFACE NUMBER	BETA-	BETA- MAX	GAMMA- MIN	GAMMA-	PSI	THETA	PHI
26	-42.800	.000	144.380	180.000	-102.050	-90.000	.000
27	-42.800	.000	180.000	215.620	-77,950	90.000	•000
28	-26.000	26.000	.000	84.000	•000	6000	•000
29	-19.000	19.000	-22.000	.000	•000	€000	•000
30	-10.000	10.000	-22.000	.000	.000	4000	•000
31	-19.000	19.000	.000	39.800	.000	6000	•000
32	45.750	64.750	9.000	25.800	.000	.000	-90.000
33	-64.750	-45.750	154.200	171.000	.000	6000	90.000
34	•000	18.000	.000	30.000	.000	4000	-90.000
35	-18.000	•000	.000	30.000	.000	6000	90.000
36	-80.000	•000	166.630	193.370	90.000	6000	5.367
37	•000	84.000	.001	360.000	13.370	954367	•000
38	•000	84.000	.001	360.000	-13.370	95.367	•000
39	-357.000	-292.200	167.590	174.750	90.000	906000	-13.370
40	-357.000	-292.200	185.250	192.410	90.000	-906000	-13.370
41	-112.400	-47.800	166.000	194.000	90.000	.000	13.100
42	-17.100	•000	113.750	174.750	90.000	906000	-13.370
43	-17.100	•000	185.250	246.250	90.000	-90.000	-13.370
44	-115.900	-73.600	174.550	185.450	90.000	•000	66.900
45	98.500	300.000	.001	360.000	.000	96.817	•000
. 46	.001	180.000	.001	360.000	.000	6000	.000
47	125.000	300.000	.001	360.000	.000	95,367	•000
48	•000	10.400	.001	360.000	•000	•000	-90.000
49	-2,630	2.640	-31.000	31.000	.000	304000	-90.000
50	-38.620	38.620	-18.000	.000	.000	6000	•000



Table 2-1. OH-58 Helicopter Geometrical Structure Data (Cont'd)

SURFACE HELICOPTER PART NUMBER DESCRIPTION	SURFACE TYPE	FLIGHT STATION	WATER-	BULKHE	AD ALPHA
51 UPPER VERTICAL STABILIZ.	TRAPEZOID	-393.030	197.380	.000	.000
52 LOWER VERTICAL STAB	TRAPEZOID	-411.580	-14.200	.000	.000
53 FRONT OF SAIL	SPHERE	-73.000	72.000	.000	11.000
54 L. FWD SIDE OF SAIL	CYLINDER	-73.000	72.000	.000	11.000
55 R. FWD SIDE OF SAIL	CYLINDER	-73,000	72.000	.000	11.000
56 FWD TOP OF SAIL	TRAPEZOID	-73.000	83.000	.000	.000
57 SAIL	CYLINDER	-109.230	94.000	.000	10.000
58 FRONT TOP OF SAIL	DISC	-109.230	94.000	.000	.000
59 TOP OF SAIL	RECTANGLE	-109.230	94.000	.000	.000
60 L. INTAKE	RECTANGLE	-109.230	94.000	10.000	.000
61 R. INTAKE	RECTANGLE	-109.230	94.000	-10.000	•000
62 L. SIDE OF SAIL	RECTANGLE	-121.000	94.000	15.000	.000
63 R. SIDE OF SAIL	RECTANGLE	-121.000	94.000	-15.000	.000
64 ROTOR HUB	CYLINDER	-107.130	118.000	.000	1.250
65 ROTOR	RECTANGLE	-107.130	118.000	.000	.000
66 TOP ENGINE COWLING	TRAPEZOID	-221.000	94.000	.000	•000
67 L. SIDE ENGINE COWLING	RECTANGLE	-121.000	94.000	15.000	.000
68 R. SIDE ENGINE COWLING	RECTANGLE	-121,000	94.000	-15.000	.000
69 TOP AFT ENG. COWLING	TRAPEZOID	-215.840	80.840	.000	.000
70 L. AFT ENG. COWLING	TRAPEZOID	-240.200	75.000	-4.000	.000
71 R. AFT ENG. COWLING	TRAPEZOID	-240,200	75.000	4.000	.000
72 REAR ENGINE COWLING	RECTANGLE	-200,600	84.500	.000	•000
73 L. BOTTOM TAIL PIPE	CYLINDER	-138.000	100.000	13.500	3.000
74 R. BOTTOM TAIL PIPE	CYLINDER	-138.000	100.000	-13.500	3.000
75 L. BEND IN TAIL PIPE	SPHERE	-138.000	100.000	13.500	3.000



Table 2-1. OH-58 Helicopter Ceometrical Structure Data (Cont'd)

SURFACE NUMBER	BETA- MIN	BETA- MAX	GAMMA-	GAMMA-	PSI	THETA	PHI
51	66.300	111.200	16.000	25.000	.000	6000	-90.000
52	-106.200	-77.080	146.500	155.000	.000	6000	-90.000
53	.001	90.000	.001	180.000	•000	6000	•000
54	•000	53.100	.001	360.000	-4.700	-90.000	•000
55	•000	53.100	.001	360.000	4.700	-90:000	•000
56	•000	49.000	175.300	184.700	-90,000	•000	•000
57	-15.000	.000	.001	360.000	•000	•000	•000
58	•000	15.000	.001	180.000	.000	6000	•000
59	-15.000	15.000	-11.770	.000	.000	. 6000	•000
60	•000	7.070	.000	20.000	•000	906000	-45.000
61	-7.070	.000	.000	20.000	.000	906000	45.000
62	•000	20.000	.000	6.770	.000	•000	-90.000
63	-20.000	•000	.000	6.770	•000	6000	90.000
64	-30.000	•000	.001	360.000	•000	5.000	•000
65	-6.510	6.520	-212.000	212.000	45.000	1.650	1.650
66	-100.000	-60.000	171.460	188.540	90.000	.000	•000
67	•000	40.000	.000	25.000	.000	906000	-98.540
68	-40.000	.000	.000	25.000	•000	906000	98.540
69	-56.390	-15.690	170.930	189.070	90.000	6000	-13.500
70	-80.200	-40.100	180.000	193.500	90.000	90.000	-9.070
71	-80.200	-40.100	166.500	180.000	.90.000	-90:000	-9.070
72	-2.500	2.500	-6.333	•000	.000	-906000	•000
73	-12.000	.000	.001	360.000	.000	6000	-45.000
74	-12.000	.000	.001	360.000	•000	.000	45.000
75	•001	180.000	.001	360.000	.000	•000	•000



Table 2-1. OH-58 Helicopter Geometrical Structure Data (Cont'd)

SURFACE HELICOPTER PART NUMBER DESCRIPTION	SURFACE TYPE	FLIGHT WATER- STATION LINE	BULKHEAD ALPHA
76 R. BEND IN TAIL PIPE	SPHERE	-138.000 100.000	-13.500 3.000
77 L. BACK OF TAIL PIPE	CYLINDER	-138.000 100.000	13.500 3.000
78 R. BACK OF TAIL PIPE	CYLINDER	-138.000 100.000	-13.500 3.000
79 L. END OF TAIL PIPE	DISC	-138.000 100.000	13.500 4.000
80 R. END OF TAIL PIPE	DISC	-138.000 100.000	-13.500 4.000



Table 2-1. OH-58 Helicopter Geometrical Structure Data (Cont'd)

SURFACE . NUMBER	BETA- MIN	BETA- MAX	GAMMA- MIN	GAMMA-	PSI	THETA	PHI
76	.001	180.000	.001	360.000	.000	6000	•000
77	•000	4.000	.001	360.000	.000	-90.000	•000
78	•000	4.000	.001	360.000	.000	-90.000	•000
79	.000	3.000	.001	360.000	.000	-90.000	•000
80	•000	3.000	.001	360.000	.000	-90.000	•000



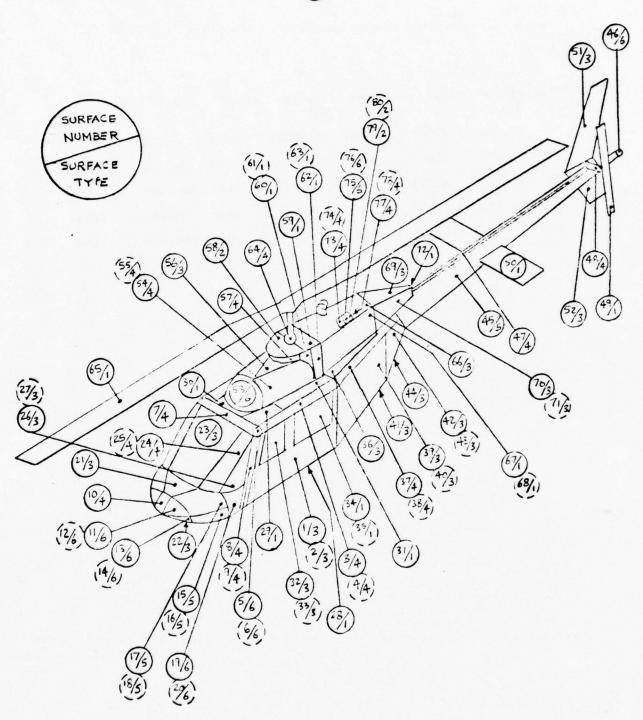
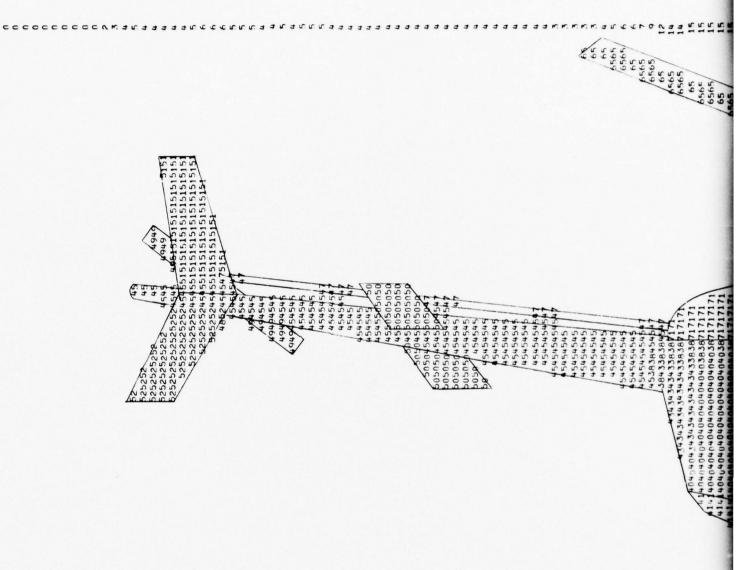
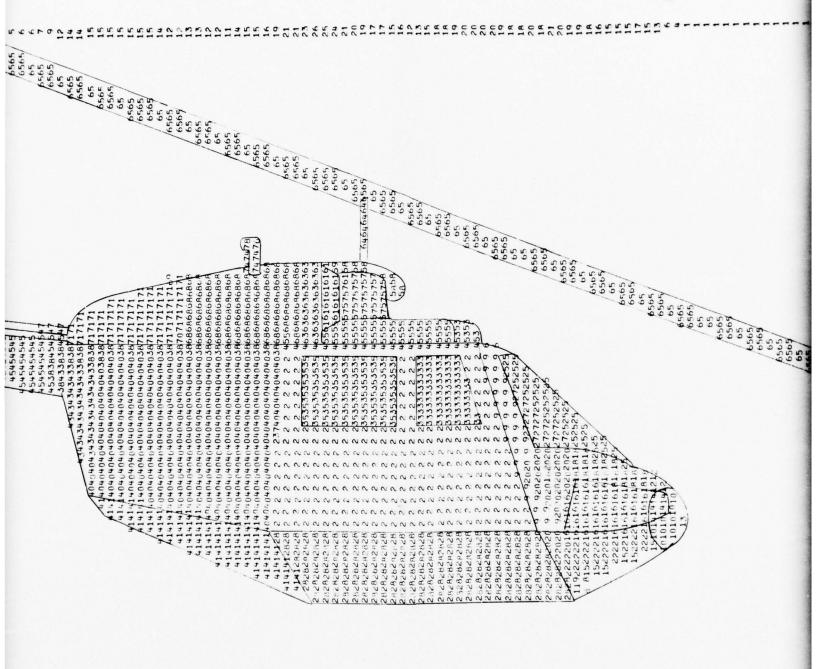


Figure 2-1. OH-58 Surface Locations

2-10







2009

Figure 2-2. (U) OH-58 Printout @ 70° Aspect Left Roll

2-11/2-12



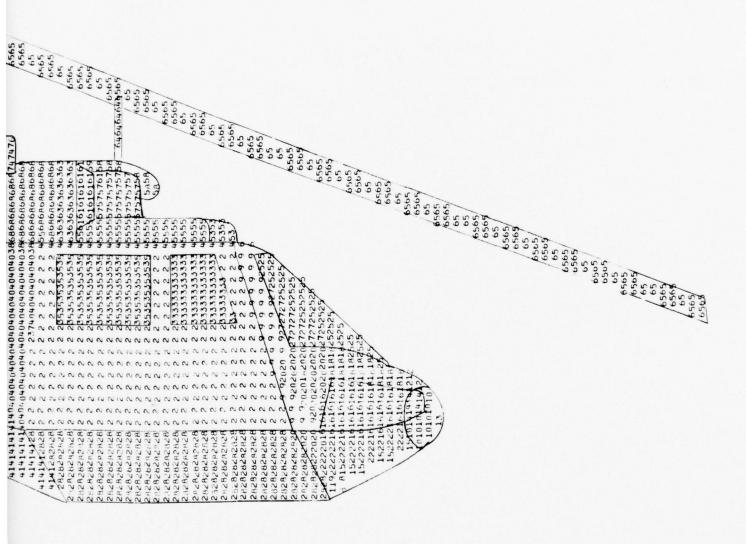


Figure 2-2. (U) OH-58 Printout @ 70° Aspect With 20° Left Roll

2-11/2-12

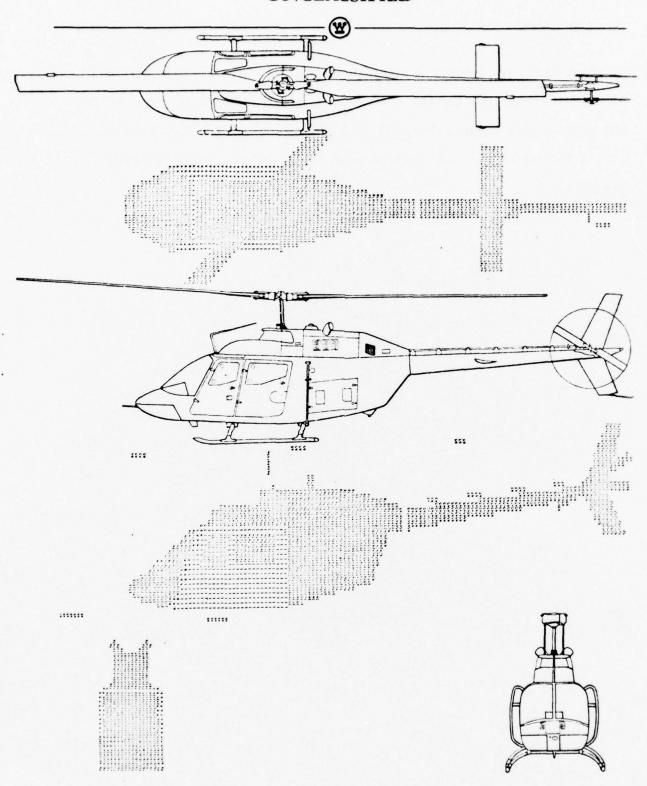


Figure 2-3. (U) OH-58 Silhouette Comparisons

2-13



printout have been reduced in size to the scale of a three view drawing from an OH-58 manual. The individual numbers have become too small to read, but the silhousettes compare favorably with those of the three view drawing.

A listing of the body Block Data in the HIDE Model is presented in Appendix A.

#### UNCLASSIFIED



#### 3.0 (U) HELICOPTER OPERATING CHARACTERISTICS AND TURBINE DATA

The Hide Model requires certain data which describes the plume exit from the tailpipe. This data is computed in an off-line program using inputs which describe the helicopter operating characteristics and the turbine. The input data for the off-line program is presented in tabular form in this section. A listing of the off-line program and its block data are presented Appendix B.

#### 3.1 (U) HELICOPTER OPERATING CHARACTERISTICS

The operating characteristics for the OH-58 helicopter are presented in tabular form in Tables 3-1 through 3-3. Table 3-1 presents speed and torque data as a function of pressure altitude for cruise speed. Tables 3-2 and 3-3 present similar data for maximum cruise speed and hover respectively.

The original data from the OH-58 Operator's Manual from which Tables 3-1 to 3-3 were generated are shown in Appendix C. They include specific range curves showing true airspeed and fuel flow as a function of gross weight and pressure altitude, maximum cruise curves showing airspeed limitations as a function of gross weight and air temperature, fuel flow curves showing torque pressure as a function of fuel flow and pressure altitude, and torque and power required to hover curves showing torque pressure and shaft horsepower requirements for hovering as a function of gross weight and density altitude.

#### UNCLASSIFIED



#### 3.2 (U) TURBINE DATA

The AH-1G uses one Allison Model T63-A-700 turbine. The data from this engine are presented in tabular form in Tables 3-4 through 3-6. Table 3-4 shows air flow (Wa), fuel flow (Wf) and net thrust (Fg) for various combinations of altitude and shaft horsepower (SHP) settings. Table 3-5 shows Turbine outlet temperature versus shaft horsepower. Table 3-6 presents correction factors for air flow, fuel flow, and net thrust as a function of ambient temperature.

The original data from the Allison manual from which tables 3-4 through 3-6 were generated is shown in Appendix D. They include performance curves for altitudes of 0, 5000, 10,000 15,000 and 20,000 feet, and an ambient temperature correction curve.



Table 3-1. OH-58 Helicopter Speed and Torque Data for Cruise Speed

	Gross Weight	: 1500 Lbs.	Gross Weight:	2000 Lbs.
Pres. Alt. (Ft.)	Torque Pres. (PSIG)	Speed (Knots)	Torque Pres. (PSIG)	Speed (Knots)
0 2000 4000 6000 8000 10000 12000 14000 16000 18000 20000	53 50 47 44 43 41 39•5 38 38 38 34	1035 104 104 104 104 1035 103 103 102 99 94	55 54 53 50 49 46 45 43 42 40 38	103 104 104 104 104 104 1035 103 103 99 94
	Gross Weight:	2500 Lbs.	Gross Weight:	3000 Lbs.
Pres. Alt. (Ft.)	Torque Pres. (PSIG)	Speed (Knots)	Torque Pres. (PSIG)	Speed (Knots)
0 2000 4000 6000 8000 10000 12000 14000 16000 18000 20000	60 60 58 55 55 52 52 49 47 43 40	103 103.5 103.5 103.5 104 104 103 98 .93 83 73	70 65 62 61 59 55 51 47 47 45	102.5 103 103 102 97.5 91.5 83 74 64 58 37.5



Table 3-2. OH-58 Helicopter Speed and Torque Data for Maximum Cruise Speed

	Gross Weight	t: 1500 Lbs.	Gross Weight	t: 2000 Lbs.
Pres. Alt. (Ft.)	Torque Pres. (PSIG)	Speed (Knots)	Torque Pres (PSIG)	Speed (Knots)
0 2000 4000 6000 8000 10000 12000 14000 16000 18000 20000	53 60 60 58 53 48 45 40 38 34 30	117 117 120 120 118 115 112 107 103 99 94	65 64 61 59 57 52 49 47 44 40 38	115 116 116 115 115 114 112 107 103 99 94
	Gross Weight Torque Pres. (PSIG)		Gross Weight Torque Pres. (PSIG)	
0 2000 4000 6000 8000 10000 12000 14000 16000 18000 20000	71 68 64 61 59 55 52 49 47 43 40	111.5 112.5 111 111 109.5 106.5 103 98 93 83 73	69 68 64 61 59 55 51 47 47 45	106.5 106.5 104 102 97.5 91.5 83 74 64 58



Table 3-3. OH-58 Helicopter Speed and Torque Data for Hover

	Gross Weight:	1500 Lbs.	Gross Weight:	2000 Lbs.
Pres. Alt. (Ft.)	Torque Pres. (PSIG)	Speed (Knots)	Torque Pres. (PSIG)	Speed (Knots)
0 2000 4000	30 32 34	0 0	45 46 46	0 0
6000 8000 10000	35 36 36	0 0 0	46 47 48	0 0
12000 14000 16000	38 39 40	0 0 0	49 50 51	0 0 0
18000 20000	40 41	0	51 52	0

	Gross Weight:	2500 Lbs.	Gross Weight:	3000 Lbs.
Pres. Alt. (Ft.)	Torque Pres. (PSIG)	Speed (Knots)	Torque Pres. (PSIG)	Speed (Knots)
0 2000 4000 6000 8000 10000 12000 14000 16000 18000 20000	58 59 60 61 62 63 64 66 68 72 76	0 0 0 0 0 0 0 0 0 0 0 0	73 74 75 77.5 80 82.5 86 90 95 100 110	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0



	Table 3-4.	Engine Parar	neters at S	tandard Ambient	t Temperature	
	Altit	cude: Sea Le	evel	Altitud	ie: 5000 Fee	t
SHP	Wa (1b/sec)	Wf (lb/hr)	Fg (1b)	Wa (lb/sec)	Wf (lb/hr)	Fg (1b)
50 100 150 200 250 300	2.14 2.43 2.65 2.83 3.0 3.14	85 105 127.5 152 177.5 205.5	7.5 12 16 21 26 32	1.9 2.12 2.35 2.51 2.66 2.76	75 93 117 144 172.5 207	7.5 12 16 21 26 32
	Altitu	de: 10,000	Feet	Altitu	de: 15,000	Feet
SHP	. Wa (lb/sec)	(lb/hr)	Fg (1b)	Wa (1b/sec)	Wf (lb/hr)	Fg (1b)
50 100 150 200 250 300	1.45 1.88 2.08 2.23 2.33 2.39	65 86 111 138 172.5 207	7 11 16 21 26 32	1.44 1.66 1.83 1.95 2.095 2.04	60 80 105 138 171 204	7 11 16 21 26 32

	Altitu	de: 20,000 Feet	
SHP	Wa	Wf	Fg
	(1b/sec)	(lb/hr)	(1b)
50	1.25	50	6
100	1.45	75	11
150	1.6	103.5	16
200	1.65	140	21



Table 3-5. Referred Power Turbine Outlet Total Temperature Versus Referred Shaft Horsepower

SHP/ amb eamb	Tto/9amb*	
150	1757	
150 175	1763 1770 1778	
200 225 250 275	1770	
225	1778	
250	1786 1794 1803	
275	1794	
300	1803	

\*Note:  $\theta_{amb}$  = relative temperature ratio =  $\frac{T_{amb}}{519}$  @ altitude ( ${}^{\circ}$ F)

Table 3.6. Ambient Temperature Correction Factors (100% normal rated power)

Tamb ( <sup>O</sup> R)	<u>Wa</u> Wa	Wf Wf	Fg amb
420	0	0	0
440	0	0	0
460	0	0	0
480	0	0	0
500	0	0	0
520	0	0	0
540	0	! 0	. 0
560	0	0	0
420 440 460 480 500 520 540 560 580	0	0	0



#### 4.0 (U) OH-58 SIGNATURE

The OH-58 surface data derived and listed in Table 2-1 was put into the HIDE model in the form of "block data" as given in Appendix A. The OH-58 turbine model (listed in Appendix F) was then run off line to derive inputs for the HIDE model. Neteorlogic and operating conditions were selected and the HIDE program executed to generate an OH-58 signature.

The generation of a viable signature represents the completion of the CH-58 model construction. This section describes a typical signature.

#### 4.1 (U) INPUT DATA

The input data that was used to obtain the sample signature is given in Table 4-1.

The identification of the variable names and their units are as follows:

TAIR = Ambient air temperature, degrees Kelvin

PRESS = Ambient pressure, millibars

RMIX = Mixing ratio, gms H<sub>2</sub>O/Kgm dry air

VISR = Visual range, M1

CFRA = Cloud fraction, tenths

IDAY = Flag, l = night, 2 = day

AZSUN = Azimuth of sun relative to LOS, degrees

ZESUN = Zenith of sun, degrees
WINDVL = Wind velocity, ft/sec

WANGLE = Compass heading of wind origin, degrees

RGND = Reflectivity of ground EGND = Emissivity of ground TGND = Temperature of ground RCLD = Reflectivity of cloud

HT = Helicopter height, KM

PSIH = Helicopter yaw relative to East, degrees

THETAH = Helicopter pitch, degrees
PHIH = Helicopter roll, degrees
SPEEDH = Helicopter speed. ft/sec

SPEEDH = Helicopter speed, ft/sec YAWV = Helicopter velocity vector yaw relative to air

frame, degrees

PITCHV = Helicopter velocity vector pitch relative to air

frame, degrees

ROLLV = Helicopter velocity vector roll relative to air frame, degrees



ALT	Atmospheric p	ressure, atmospheres
AIRTHP		re at helicopter altitude, deg. Kelvin
FEFF	Combustion ef	
FHTOC		arbon ratio of fuel
FATOMS		bon atoms in fuel molecule
QQ1	1 + fuel to a	
XTMP		
	Exit gas temp	
AIRH2O		ure of water vapor in air, percent
AIRCO2		ure of carbon dioxide in air, percent
XH20		ure of water vapor in exhaust gas,
1.000	percent	
XC02		ure of carbon dioxide in exhaust gas
ATDOD	percent	
AIRCP	Specific heat	
EXVEL		xit gas, ft/sec
DOWNSH	Down wash vel	
DE	Exit diameter	, inches
R	Range, KM	
HO	Observer Heig	
HX	Helicopter po	attion in earth coordinate system
	(EAST), inche	
HY	Helicopter po	sition in earth coordinate system
	(NORTH), inch	
HZ	Helicopter po	sition in earth coordinate system
	(ELEVATION),	inches
OX	Observer posi	tion in earth coordinate system
	(EAST) inches	
OY	Observer posi	tion in earth coordinate system
	(NORTH), inch	
OZ		tion in earth coordinate system
	(ELEVATION),	
PSIO	LOS yaw angle	
THETAO	LOS pitch ang	
PHIO	LOS roll angl	
TPTNP	Temperature o	
TPEMS	Emissivity of	
COVER		suppressor, 1 = suppressor
FOVX		d of view in azimuth, degrees
FOVY		d of view in elevation, degrees
ANGX		ution in azimuth, degrees
ANGY		ution in elevation, degrees
LOW	Short wave le	
LHI	Long wave len	
BIASK		acements of LOS from center of gravity,
DIAGI	resolution el	
BIASJ		placement of LOS from center of gravity,
	resolution el	ements
CHIT	Cloud height	
ECLD	Emissivity of	
PRD	Log plot scal	e factor

DATA
INPUT
9
4-1.
TABLE

-	38D 08-53	SPECT 230	
TAIN =	.28700000785.	PRESS = .131300001+34	41X = .272556. CE+61
CS I	0+30000000	FD 1 C.	DAY = .20066
KDS7	31900300E+0	EASUNE . CASOSOSOSOS	1NDVL= .110000000 = 0
ALGLE	د،	GND = .7000000E-0	GND = .93000000E+0
CNS	873C3CGE+C	CL3 =13000000E+0	T(1) = .12500030E-0
RIS	.610003695+32	HETAH = 17000000E+	HIH =300000006E+0
PEEDH		AWV = C.	ITCHV= 0.
0110		TM = .91700000E+C	IRTMP= .287000.000+0
333	.95000000E+9	HIOC = .200000000E+0	ATOMS= .74803030E+9
9	0154000E+C	TMP = .38400900E+0	IRH20= .10060000E-0
19002	201035CE-0	H20 = .80000000E-0	CO2 = .30000000E-0
30	26600000000000	IRCP = .24000320E+0	XVEL = .25000000E+3
DWNSH	1030:30 0F + 0	6055550° = 3	0-3390003000 = (1)
0(1)	.10.60000E-02	x = .33200000E+C	+ 3000000000 = . Y
2	950000000	• ii ×	.0 = 0.
2	3937000JE+0	SIO = .116u8930E+6	HETAG= 0.
OIH	•	PTMP = .83100030E+0	1+30:10000+ = SW30
COVED	•	OVX = .27.30030E+6	. 17506C.
NOX	.700000007.	3 -3000000000 = YOU	OW = .200000000000
H	650000000E+4	DARK = .1000000001.	IASJ = . ACOUGEUGE+C
HIT	100000001	GLD = .100033690E+3	RD = 445455655656
0.0	000.0	39.3761 10.911	-7.6259 93.030
	5.00.000	92.1260 61.000	17.0000 -30.000
5.5	364.4	. 1766	0000 10.000
707	CCE+03 .154 300	F-01 .29831195E-01 .334	50435-0
0192	30E+33 .103333	7+025.	0+30000
69593	0	.996194705+10 .871	5741E-0
550	73E+31 .346319	C+12 .22762017E+	
7007	955 + 34	C+12 . 83175696F+C	



#### 4.2 (U) LOG PLOT SIGNATURE

The signature predicted for these initial conditions is shown in figure 4-1. This figure depicts the spatial intensity distribution of the signature.

The picture consists of a mosaic of 30 by 60 elements. The apparent effective radiance of each element is depicted by a 2 digit number. The first digit represents the characteristic of the logarithym of the radiance multiplied by a scale factor and the second digit the first number of the mantissa.

The value of the radiance is typically less than unity. Therefore it is multiplied by a scale factor PRD. If the product of the radiance times PRD was 267.5, then its logarithm would be  $\log 10 \ (267.5) = 2.4273$ , which when rounded off to the first decimal and multiplied by 10, becomes 24. Thus, the two digit value printed out for this surface intercept would be 24.

The advantage of using logarithms is in obtaining a large dynamic range with the fewest digits. For example, the surface radiances in figure 4.1 are in the twenties, while the hot gas values are in the forties. This indicates at a glance that the hot gas is two orders of magnitude more radiant than the surface.

The background radiance values have been suppressed for picture clearity except for the last column and row. This permits determining at a glance what the background level is and if there are any gradients present.

At the bottom of the picture frame are three lines of real numbers which define aspects of the integrated signature in various ways.

The first line gives the components of contrast irradiance which comprise the composite signature. The first number is the total positive contrast irradiance, the second number is the total negative contrast irradiance and



		1535759545	14939343226252123;	
	25?	5252525252	50525252525252525	2525 25
			62626262625252525	
			6272726262626252525	
	252		62727262726262626	
	252		62627262736373534	
	252		42636363A37353525	
			43333363837272626	
			53631363427272726	
	25252		72833332828272726	
	25252		73636332828272726	
	25252		828353: 1232272426	
	25252		#343528282726262625	
	252521		3393528282726262625	
			736352828272625252	
			136342827272625252	
	252525?		73534282726252525	
	2525252	7293129293	915292827262525252	
	2525252	8333029293	13429282726252525	25
	25252629	9313029293	734324126252525	25
26	2525273	0313029373	533383926252525	25
26			+323939362525	25
26			3352437353125	25
26			33527373331	25
26			63526253226	25
26			53225252526	25
26		4323635343		25
2626		32 332 33322 130 33333312		25
26		9313433312		25 1
26		333533292		25
26		353632272		25
26			52626262626	25
2525			6262626262626	25 1
26	25424528233		52620202626252525	25 1
26	264741253241		626262626262626	25 3
25			626262626262626	25 2
26	44442527.14		626262626262626	25 2
26	474325314540	272726252		25 3
2626	_ 2850252535483 4849 25444623		12621243526252626 1202526262626262626	25 2
26 26	57342627434026		6262626262626262626	25 2 25 2
26			6262626262626262626	25 2
26			6262626262626252626	25 2
26	262558432534		626252626262626262626	25 2
2526	255748262626		6262626262626262626	25 3
26	26265757262626		62626262626262626	25 3
25	2626262526262626	5352626262	52625262525262626	25 2
26	262/3126292628	6262626262	626262626262626262	25 25 2
25272		2020202020	6262626262525262626	25 2
25	252529312626		62626252626262626	25 2
2525	262626262626			25 2
26	2626262526		526752615262626	25 2
26 • 26	2626262626		426262626262626	25 2
26	2626252526 27242626		126252626262626	25 2
26	27242626		6262626262626 6262626262626	25 2
25		242126262	5232525252525	25 2
		25262626262	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	25 2
	26 2926	252625262	12626262626	25 2
			62626262626	25 2
	26	272727272	72625252626	25 2
252525252525252	725252525252525252		626272725252525252	
\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$	55555555555555	59555555	33555	
3551355355555	35555555555555	555555555	3335	
13911157151111				
5751252535355	55345555555555	55555555	6.500	
1111111111111	1888884848484	9,155,155	22.22	
	1555555555555555	733334555	1242	
1111111111111	\$	_1,55,554,545 _1,55,5454		

FIGURE 4-1. (U) LOG PLOT SIGNATURE



the third number is the sum of the absolute values of contrast irradiance components.

The second line gives the absolute irradiance values. The first number is the absolute target irradiance, the second number is the absolute irradiance of the background covered by the target, and the third is the contrast irradiance obtained by subtracting the first two numbers.

The third line containing a single number is the apparent effective radiant intensity of the target.

In the above, the irradiance numbers have the standard units, watts/cm<sup>2</sup>, the radiant intensity, watts/ster, and the radiant values in the log plot, W/cm<sup>2</sup>/ster.

All signature values are weighted for the sensor spectral response.

#### 4.3 (U) SPECTRAL PLOT

The HDE program also prints out a plot of the spectral radiant intensity of the signature and its composition as shown in figure 4-2.

This plot is in the form of a number pattern wherein the user can connect the numbers and draw the curves.

The identification of the symbols and their priority are listed below. (i.e. If the points on more than one curve fall on the same print location, only one character is printed out overriding the others. Thus, number 1(C) would predominate over all the others, number 3(T) would prempt number 4 (R), etc.)

The vertical coordinate, calibrated from 0 to 10, represents 0 to 100 percent. The horizontal coordinate is calibrated in wavelengths. Each curve is normalized to some reference value which is printed out along the vertical coordinate and specified in Table 4-2.

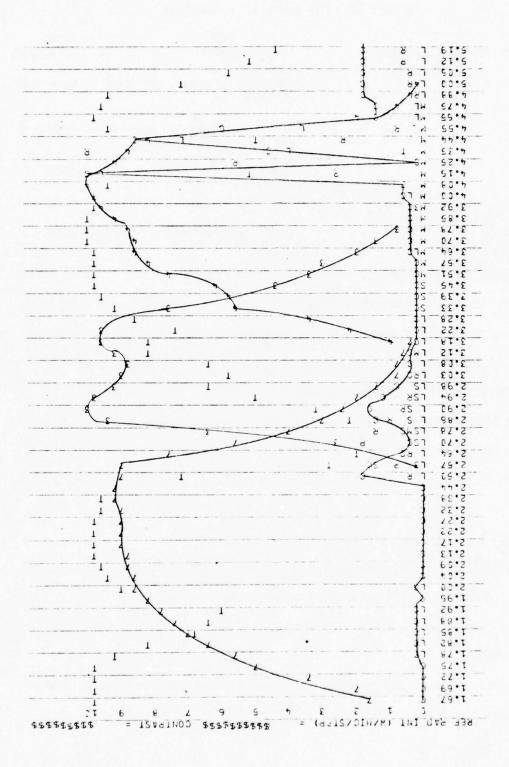


FIGURE 4-2. (U) SPECTRAL PLOT



	Table 4-2. (U) Spectral Priorities			
PRIORITY	SYMBOL	DEFINITION	REFERENCE	
1	С	Spectral radiant intensity at receiver	Contrast	
2	S,M,L	Effective apparent spectral radiant intensities	Contrast	
3	T	Atmospheric transmission	100%	
4	R	Spectral radiant intensity	Rad. Int.	
5	3,4,7	Detector responses	100%	

#### 4.4 (U) BODY INTERCEPT PLOT

A body intercept plot is also printed out as shown in figure 4-3. This is a mosaic format on a one for one correspondence with the LOG PLOT of the signature. The difference is that the 2 digit numbers given here are the index numbers of the surface elements.

Only body surfaces are shown here, the plume surfaces have been deleted. This plot may be super imposed on the LOG PLOT to investigate the origin of the signature contributions (i.e. tail boom heating, solar glint from windows, etc.).

### 4.5 (U) GREY SCALE PLOT

The HIDE model also generates a grey scale plot of the spatial distribution of intensity of the signature as shown in figure 4-4.

This is based on a 10 level grey scale using symbols to depict the density levels.

This plot enables one to find hot spots quickly and track them through the BODY and LOG PLOTS.



1			2
2		4546 52	3
4	The same of the sa	45 525252	4
. 5		51515151514949 45 5252525252	5
6		51515151515149514551525252	6
7		51515151514949455252	
8		515151494552 	8
10		474549	10
11		454349	11
12		454549	12
13		45434949	13
14		5050 4545	14
15		5050 4545 505J474545	15 16
17		51474545	17
18		50504545	18
19		504545	19
20		454545	20
21	65	45455050 4745455050	25
23		474545505050	23
24		4545 505050	24
25	65	4545 505050	25
26	65	434545 5050	26 27
27	65	454545 50 47454545	28
	5565	47454545	29
30	65	454545	30
31	55	454545	31
32	65	4545454	32
33	65	474545454444444444	33
35	6565	697070373744444444444	35
36	65	696372373742424244444444	36
37	65	69707037373742424242424244	37
38	65	69697273373737424239393939393	38
39	65	6969697373737393939393939393939 66636970737373939393939393939	39_
40	6565	666969707070373739393939393939393941	41
42	65	6666707070703737393939393939393939	42
43	55	789066666676767673737343939393939393939	43
44	65	7474746666676767673737393939393939393939	44
45	65	6666666676767676737373939393939393939393	45
46	65 6565	597779676767676737373939393939393939393	47
48	65	585975775767676757373739393939393939393939	48
49	65	58595966676767676767373739393939393939393939	43
50	65	58645959676767623137373939393939393939 1 1	50
51		5859596252626231 3373939 1 1 1 1 1 1 1 1 1 1 58595757545454 3 3 3 1 1 1 1 1 1 1 1 1 1	51 52
52	65 6565	58585757545454 3 3 3 1 1 1 1 1 1 1 1 1 1 58585754545431 3 334343434 1 1 1 1 1 1 1	53
54	65	45454545431 3 334343434 1 1 1 1 1	54
55	65	555454545431 3 334343434 1 1 1 1 1	55
56	65	5354545431 3 3 3343434 1 1 1 1 1 1	56
57	65	53545429 3 3343434 1 1 1 1 1 1	57_
58	65	312929 3 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	58 53
59	65 65	29 3 3 332323232 1 1 1 1 1 1 7 7 332323232 1 1 1 1 1 1	60
61	65	24 3 3 1323232 1 1 1 1 1	61
£2	65	24 52626 1 1 1 1 1 1 1	6.2
63	65	24242526131919_1 1 1	6.3
€4			64

FIGURE 4-3. (U) BODY INTERCEPT PLOT



#### 4.6 (U) GREY SHADE PLOT

Data from the log plot signature is used in an off line program to generate a grey shade plot as shown in figure 4-5. It depicts the same information as the grey scale plot, but in a way which provides a truer visualization of the grey shade densities. This effect is obtained by use of an overprint process.

#### 4.7 (U) GREY SHADE PHOTO

This photograph, shown in figure 4-6, is a simulation of what an infrared camera would see when looking at the target. It was obtained by processing the digital signature image mosaic. The special intensity distribution values from the log plot signature were fed through a hybrid computer's D/A converter to convert digital values to analog video amplitudes. The video amplitudes were then displayed on a kinescope and photographed. The capability of generating photographs of this type is an inherent feature of the digital mosaic techniques used in the HIDE model.



	2
	****:::
::::: ********	
!!!!!!!!!	
1:++++::++++	
!:+++	14
	15
::++++++	16
!:+!!	17
++++	19
++::	20
	21
::+++	22
!!!!!!!++++*	23
!!!!!!!!!!	
11111111++++++ 11	26
111111111111	27
11++11++1111	2.8
	29
++++1	30
11+++::::++::	31
++++11+++11	33
02++1: + + + +	34
++05+++++::	35
0000+++::	36
1:00:: ++00++	37
0000++30	39
\$80033++	40
3:	41
0015 0000	42
++++00++	43
**************************************	44
++C3	45
++00	47
++++	48
	49
	50
	51
11	52 53
and the state of t	54
	55
A CONTRACT OF THE RESIDENCE OF THE PARTY OF	56
	57
	58
	59
	50
	61
	63
**	64

GREY SCALE PLOT

<u>(a)</u>

FIGURE 4-4.

4-11



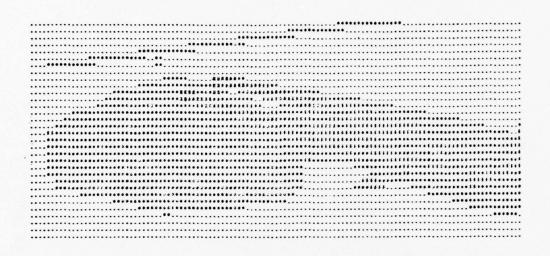


Figure 4-5. (U) Grey Shade Plot



Figure 4-6. (U) Grey Shade Photo

4-12



APPENDIX A (U)

BLOCK DATA FOR BODY IN THE HIDE MODEL



OHDATA -- PAGE 1 14.50.56 73/09/25 80 8 64 79 1 -121.000 192.900 26.000 127.900 173.900 ·001 25.800 ·000 ·000 ·000 -90.000 3 1 2 -121.000 192.900 -26.000 -173.900 -127.900 154.200 180.000 .000 .000 .000 90.000 3 1 3 -59.200 65.000 19.000 .000 63.000 ·001 360·000 7·000 ·000 -90·000 ·000 4 1 4 -59.200 65.000 -19.000 .000 63.000 ·001 360·000 7·000 ·000 -90·000 ·000 4 1 5 -59.200 65.000 19.000 .001 180.000 ·001 360·000 7·000 ·000 ·000 ·000 6 1 6 -59.200 65.000 -19.000 .001 180.000 ·001 360·000 7·000 ·000 ·000 ·000 6 1 7 -59.200 65.000 .000 -19.000 19.000 ·001 360·000 7·000 ·000 ·000 90·000 4 1 8 -59-200 65-000 19-000 -000 51-000 180.000 360.000 7.000 .000 154.200 .000 4 1 9 -59.200 65.000 -19.000 .000 51.000 180.000 360.000 7.000 .000 154.200 .000 4 1 10 -8.000 33.000 .000 -7.000 7.000 ·001 360·000 7·000 ·000 ·000 90·000 4 1 11 -8.000 33.000 7.000 .001 90.000 ·001 180·000 7·000 90·000 ·000 ·000 6 1 12 -8.000 33.000 -7.000 .001 90.000 90.000 270.000 7.000 .000 .000 .000 6 1 13 -8.000 33.000 7.000 90.000 180.000 ·001 180·000 7·000 90·000 ·000 ·000 6 3 14 -8.000 33.000 -7.000 90.000 180.000 90.000 270.000 7.000 .000 .000 .000 6 3 15 21.000 33.000 2.000 29.400 58.800 180.000 360.000 13.400 -9.800 -90.000 .000 5 3 16 21.000 33.000 -2.000 29.400 58.800 180.000 360.000 13.400 9.800 -90.000 .000 5 3 17 21.000 33.000 2.000 29.400 58.800 ·001 180·000 13·400 -9·800 -90·000 ·000 5 1 18 21.000 33.000 -2.000 29.400 58.800 ·001 180·000 13·400 9·800 -90·000 ·000 5 1 19 -37.000 33.000 12.000 .001 180.000 ·001 360·000 14·000 ·000 ·000 ·000 6 1 20 -37.000 33.000 -12.000 .001 180.000 ·001 360·000 14·000 ·000 ·000 ·000 6 1 21 32.550 30.200 .000 -71.500 -41.700 170-890 189-110 -000 -90-000 -000 -13-400 3 1 22 32.550 35.900 .000 -71.500 -41.700 170.890 189.110 .000 -90.000 .000 13.400 3 1 23 16-440 17-720 -000 -88-900 -37-000 167.950 192.050 .000 -90.000 .000 -36.500 3 3 24 16.440 10.720 .000 38.250 90.900 ·001 360·000 7·000 -12·050 -53·500 ·000 4 3 25 16.440 10.720 .000 38.250 90.900 ·001 360·000 7·000 12·050 -53·500 ·000 4 3 26 -13.640 33.000 15.000 -42.800 .000 144.380 180.000 .000 -102.050 -90.000 .000 3

27 -13.640 33.000 -15.000 -42.800 .000 180.000 215.620 .000 -77.950 90.000 .000 3 3



OHDATA -- PAGE 2 14.50.56 73/09/25

28 -121.000 19.000 .000 -26.000 26.000 .000 84.000 .000 .000 .000 .000 1 1 29 -59.200 72.000 .000 -19.000 19.000 -22.000 .000 .000 .000 .000 .000 I 3 30 -59.200 72.010 .000 -10.000 10.000 -22.000 .000 .000 .000 .000 .000 l 1 31 -121.000 72.000 .000 -19.000 19.000 •000 39•800 •000 •000 •000 •000 1 1 32 -86.280 110.750 26.010 45.750 64.750 9.000 25.800 .000 .000 .000 -90.000 3 3 33 -86.280 110.750 -26.010 -64.750 -45.750 154.200 171.000 .000 .000 .000 90.000 3 3 34 -114.000 65.000 26.010 .000 18.000 ·000 30·000 ·000 ·000 ·000 -90·000 1 3 35 -114.000 65.000 -26.010 -18.000 .000 ·000 30·000 ·000 ·000 ·000 90·000 1 3 36 -200.600 79.500 .000 -80.000 .000 166.630 193.370 .000 90.000 .000 5.367 3 1 37 -200-600 72-500 -000 -000 84-000 ·001 360·000 7·000 13·370 95·367 ·000 4 1 38 -200.600 72.500 .000 .000 84.000 ·001 360·000 7·000 -13·370 95·367 ·000 4 1 39 -468.500 98.800 -56.500 -357.000 -292.200 167.590 174.750 .000 90.000 90.000 -13.370 3 1 40 -468.500 98.800 56.500 -357.000 -292.200 185.250 192.410 .000 90.000 -90.000 -13.370 3 1 41 -230.500 45.450 .000 -112.400 -47.800 166.000 194.000 .000 90.000 .000 13.100 3 1 42 -200.600 72.500 7.000 -17.100 .000 113.750 174.750 .000 90.000 90.000 -13.370 3 1 43 -200.600 72.500 -7.000 -17.100 .000 185-250 246-250 -000 90-000 -90-000 -13-370 3 1 44 -229.550 140.300 .000 -115.900 -73.600 174.550 185.450 .000 90.000 .000 66.900 3 1 45 -475.600 105.400 .000 98.500 300.000 •001 360·000 1·450 ·000 96·817 ·000 5 1 46 -377.660 93.550 .000 .001 180.000 ·00: 360·000 2·500 ·000 ·000 ·000 6 1 47 -474.600 108.400 .000 125.000 300.000 ·001 360·000 ·500 ·000 95·367 ·000 4 2 48 -352-180 87-180 -000 -000 10-400 ·001 360·000 1·000 ·000 ·000 -90·000 4 2 49 -352.180 96.180 10.400 -2.630 2.640 -31.000 31.000 .000 .000 30.000 -90.000 1 1 50 -270.000 79.800 .000 -38.620 38.620 -18.000 .000 .000 .000 .000 .000 1 1 51 -393.030 197.380 .000 66.300 111.200 16.000 25.000 .000 .000 .000 -90.000 3 1 52 -411.580 -14.200 .000 -106.200 -77.080 146.500 155.000 .000 .000 .000 -90.000 3 1 53 -73.000 72.000 .000 .001 90.000 ·001 180·000 11·000 ·000 ·000 ·000 6 1 54 -73.000 72.000 .000 .000 53.100 ·001 360·000 11·000 -4·700 -90·000 ·000 4 1 55 -73.000 72.000 .000 .000 53.100



OHDATA -- PAGE 3 14.50.56 73/09/25 ·001 360·000 11·000 4·700 -90·000 ·000 4 1 56 -73.000 83.000 .000 .000 49.000 175.300 184.700 .000 -90.000 .000 .000 3 1 57 -109.230 94.000 .000 -15.000 .000 ·001 360·000 10·000 ·000 ·000 ·000 4 1 58 -109-230 94-000 -000 -000 15-000 ·001 180·000 ·000 ·000 ·000 ·000 2 1 59 -109.230 94.000 .000 -15.000 15.000 -11.770 .000 .000 .000 .000 .000 1 1 60 -109.230 94.000 10.000 .000 7.070 ·000 20·000 ·000 ·000 90·000 -45·000 1 1 61 -109.230 94.000 -10.000 -7.070 .000 •000 20•000 •000 •000 90•000 45•000 1 1 62 -121.000 94.000 15.000 .000 20.000 ·000 6·770 ·000 ·000 ·000 -90·000 1 1 63 -121.000 94.000 -15.000 -20.000 .000 •000 6•770 •000 •000 •000 90•000 1 1 64 -107-130 118-000 -000 -30-000 -000 •001 360•000 1•250 •000 5•000 •000 4 2 65 -107.130 118.000 .000 -6.510 6.520 -212.000 212.000 .000 45.000 1.650 1.650 1 1 66 -221.000 94.000 .000 -100.000 -60.000 171.460 188.540 .000 90.000 .000 .000 3 1 67 -121.000 94.000 15.000 .000 40.000 ·000 25·000 ·000 ·000 90·000 -98·540 1 1 68 -121.000 94.000 -15.000 -40.000 .000 ·000 25·000 ·000 ·000 90·000 98·540 1 1 69 -215.840 80.840 .000 -56.390 -15.690 170.930 189.070 .000 90.000 .000 -13.500 3 1 70 -240-200 75-000 -4-000 -80-200 -40-100 180.000 193.500 .000 90.000 90.000 -9.070 3 1 71 -240.200 75.000 4.000 -80.200 -40.100 166.500 180.000 .000 90.000 -90.000 -9.070 3 1 72 -200.600 84.500 .000 -2.500 2.500 -6.333 .000 .000 .000 -90.000 .000 1 1 73 -138.000 100.000 13.500 -12.000 .000 ·001 360·000 3·000 ·000 ·000 -45·000 4 2 74 -138.000 100.000 -13.500 -12.000 .000 •001 360•000 3•000 •000 •000 45•000 4 2 75 -138.000 100.000 13.500 .001 180.000 ·001 360·000 3·000 ·000 ·000 ·000 6 3 76 -138.000 100.000 -13.500 .001 180.000 ·001 360·000 3·000 ·000 ·000 ·000 6 2 77 -138.000 100.000 13.500 .000 4.000 •001 360•000 3•000 •000 **-90•**000 •000 4 2 78 -138.000 100.000 -13.500 .000 4.000 ·001 360·000 3·000 ·000 -90·000 ·000 4 2 79 -138.000 100.000 13.500 .000 3.000 ·001 360·000 4·000 ·000 -90·000 ·000 2 1 80 -138.000 100.000 -13.500 .000 3.000 ·001 360·000 4·000 ·000 -90·000 ·000 2 1

LENGTH = 161 LINES



APPENDIX B (U)

TURBINE MODEL FOR

OH-58

HELICOPTER

LISTING AND BLOCK DATA

```
OHTURB -- PAGE 1
                      14.27.43
                                   73/09/25
5 PROGRAM OH58(OUTPUT)
6 PRINT. * OH-58 FLIGHT/TURBINE MODEL OPERATING CONDITIONS *
20 INTEGER THROST, HELOGW, HELOW(8)
25 INTEGER UT, TABLE
30+C THROST = THROTTLE SETTING (INTERGER)
40+C
      1 - CRUISE SPEED
50+C
       2 = MAXIMUM CRUISE SPEED
       3 = HOVER
60 +C
70 THROST=3
75+C HELOGW = HELICOPTER GROSS WEIGHT, LBS (INTERGER)
     VALUES = 1500,2000,2500,3000
80+C
85 VT=4
88 DATA(HELOW(I), I=1,4)/1500,2000,2500,3000/
89 HELOGW=HELOW(WT)
90*C A = ALTITUDE, FEET (REAL)
100 A=2000.
110*C TEMP = AMBIENT AIR TEMPERATURE, DEG CENTIGRADE (REAL)
120 TEMP=15.
130 DIMENSION HEIGHT( 13), ALT(4)
180 DIMENSION Q1T1(11), Q2T1(11), Q3T1(11), Q4T1(11)
200 DIMENSION Q1T2(11), Q2T2(11), Q3T2(11), Q4T2(11)
220 DIMENSION Q1T3(11),Q2T3(11),Q3T3(11),Q4T3(11)
260 DIMENSION VITI(11), V2T1(11), V3T1(11), V4T1(11)
280 DIMENSION VIT2(11), V2T2(11), V3T2(11), V4T2(11)
340 DIMENSION GW(3)
350 DIMENSION VEL(10), PITCH(10)
360 DIMENSION SO(6), W1(6), W2(6), W3(6), W4(6), W5(6)
370 DIMENSION U1(6), U2(6), U3(6), U4(6), U5(6)
380 DIMENSION $9(6), U9(6)
390 DIMENSION F1(6)
400 DIMENSION A0(5), T0(5), D1(5)
410 DIMENSION T2(9),C1(9),C2(9),C3(9)
420 DIMENSION R1(7), R2(7)
430 REAL LIC 5)
440 REAL MI,M2,L
450 DATA (VEL(14),14=1,10)/0.,10.,20.,30.,40.,50.,60.,70.,80.,90./
460 DATA (PITCH(14), 14=1,10)/.45,.20,-.25,-.90,-1.7,-2.5,-3.7,-5.05,
470+-6-35,-8-/
540 DATA (SO(II), II=1,6)/50.,100.,150.,200.,250.,300./
550 DATA (W1(I1), I1=1,6)/2.14,2.43,2.65,2.83,3.0,3.14/
560 DATA (W2(II), II=1,6)/1.9,2.12,2.35,2.51,2.66,2.76/
570 DATA (W3(11),11=1,6)/1.45,1.88,2.08,2.23,2.33,2.39/
580 DATA (W4(I1),I1=1,6)/1.44,1.66,1.83,1.95,2.095,2.04/
590 DATA (W5(II), II=1,4)/1.25, 1.45, 1.6, 1.65/
600 DATA (U1(12),12=1,6)/85.,105.,127.5,152.,177.5,205.5/
610 DATA (U2(12), 12=1,6)/75.,93.,117.,144.,172.5,207./
620 DATA (U3(12),12=1,6)/65.,86.,111.,138.,172.5,207./
630 DATA (U4(12),12=1,6)/60.,80.,105.,138.,171.,204./
640 DATA (U5(12), 12=1,4)/50.,75.,103.5,140./
650 DATA (F1(13),13=1,6)/7.5,12.,16.,21.,26.,32./
660 DATA (A0(14),14=1,5)/0.,5000.,10000.,15000.,20000./
670 DATA (TO(14), 14=1,5)/519.,501.,483.,465.,447./
680 DATA (D1(14),14=1,5)/.00238,.00205,.001755,.001493,.0012681 /
690 DATA (L1(14),14=1,5)/1.000,.832,.688,.564,.460/
700 DATA (T2(15),15=1,9)/420.,440.,460.,480.,500.,520.,540.,560.,580./
```



```
OHTURB -- PAGE 2
                       14.27.43
                                   73/09/25
710 DATA (C1(15),15=1,9)/0.,0.,0.,0.,0.,0.,0.,0.,0.,0./
720 DATA (C2(15), 15=1,9)/0.,0.,0.,0.,0.,0.,0.,0.,0.,0./
730 DATA (C3(15),15=1,9)/0.,0.,0.,0.,0.,0.,0.,0.,0.,0./
740 DATA (RI(16), 16=1,7)/150., 175., 200., 225., 250., 275., 300./
750 DATA (R2(16),16=1,7)/1757.,1763.,1770.,1778.,1786.,1794.,1803./
760 DATA G/32.2/
770 DATA H/ . 24/
780 DATA E/778./
790 DATA(HEIGHT(K1),K1=1,11)/0.,2000-,4000.,6000-,8000-,10000-,
800+12000.,14000.,16000.,18000.,20000./
860 DATA(Q1T2(K1), K1=1, 11)/63.,60.,60.,58.,53.,48.,45.,40.,38.,34.,30./
880 DATA(V2T2(K1), K1=1,11)/115.,116.,116.,115.,115.,114.,
890+112.,107.,103.,99.,94./
900 DATA(Q2T2(K1), K1=1,11)/65.,64.,61.,59.,57.,52.,49.,47.,44.,40.,38./
920 DATA(V3T2(K1),K1=1,11)/111.5,112.5,111.,111.,109.5,106.5,
930+103.,98.,93.,83.,73./
940 DATA(Q3T2(K1),K1=1,11)/71.,68.,64.,61.,59.,55.,52.,49.,47.,43.,40./
960 DATA(V4T2(K1),K1=1,11)/106.5,106.5,104.,102.,97.5,91.5,
965+83.,74.,64.,58.,37.5/
970 DATA(Q4T2(K1),K1=1,11)/69.,68.,64.,61.,59.,55.,51.,47.,47.,45.,40./
1250 DATA (VITI(K1), K1=1,11)/103.5,104.,104.,104.,104.,103.5,
1260+103.,103.,102.,99.,94./
1270 DATA(QIT1(K1),K1=1,11)/53.,50.,47.,44.,43.,41.,39.5,38.,38.,34.,
1280+30-/
1290 DATA(V2T1(K1),K1=1,11)/103.,104.,104.,104.,104.,104.,
1300+103.4,103.,103.,99.,94./
1310 DATA(Q2T1(K1),K1=1,11)/55.,54.,53.,50.,49.,46.,45.,43.,42.,40.,38/
1330 DATA(V3T1(K1),K1=1,11)/103.,103.,103.5,103.5,104.,104.,
1340+103.,98.,93.,83.,73./
1350 DATA(Q3T1(K1),K1=1,11)/60.,60.,58.,55.,55.,52.,49.,47.,43.,40/
1370 DATA(V4T1(K1),K1=1,11)/102.5,103.,103.,102.,97.5,91.5,
1375+83 . . 74 . . 64 . . 58 . . 37 . 5/
1380 DATA(Q4T1(K1),K1=1,11)/70.,65.,62.,61.,59.,55.,47.,47.,45.,40./
1470 DATA(V1T2(K1),K1=1,11)/117.,117.,120.,120.,118.,115.,
1480+112.,107.,103.,99.,94./
1510 DATA(Q1T3(K1),K1=1,11)/30.,32.,34.,35.,36.,37.,38.,39.,40.,40.,414
1550 DATA(Q2T3(K1),K1=1,11)/45.,46.,46.,46.,47.,48.,49.,50.,51.,51.,524
1590 DATA(Q3T3(K1),K1=1,11)/58.,59.,60.,61.,62.,63.,64.,66.,68.,72.,764
1620 DATA(Q4T3(K1),K1=1,11)/73.,74.,75.,77.5,80.,82.5,
1630+86 . . 90 . . 95 . . 100 . . 110 . /
1701 DATA PI/3.1415926535/
1702 DATA DTR/0.0174532925/
1703
      DATA CHORD/1.0859/
1704
      DATA BLADES/2./
     DATA RADIUS/17.667/
1705
     DATA ROTSPD/5.9/
1706
1707
      DATA DRAG/0.0083/
     DATA PLREFF/0.85/
1708
1709
     DATA TILT/0./
1710 T = 15. - 2. +A/1000.
1720 D=TEMP-T
1730 B=-(D+25.)*D*(D-10.)*(D-30.)*(D-40.)/15./40./50./70./80.
1740 B=B+3.28571
1750 B=B+(D+40.)+D+(D-10.)+(D-30.)+(D-40.)/15./25./35./55./65.+2.
1760 B=B-(D+40.)*(D+25.)*D*(D-30.)*(D-40.)/50./35./10./20./30.
```



```
OHTURB -- PAGE 3
                        14.27.43
                                     73/09/25
1770 B=B+(D+40.)*(D+25.)*D*(D-10.)*(D-40.)/70./55./30./20./10.*2.71429
1780 DELP=B-(D+40.)*(D+25.)*D*(D-10.)*(D-30.)/80./65./40./30./10.*3.571
1790 A = A + 1000. *DELP
1800 T = TEMP+9./5.+492.
1820 TABLE = (THROST-1 )*4 + WT
1830 GO TO (1,2,3,4,5,6,7,8,9,10,11,12), TABLE
1850 1 CALL CONFRACII, HEIGHT, VITI, A, V)
1860 CALL CONFRACII, HEIGHT, QITI, A, Q)
1870 GO TO 199
1880 2 CALL CONFRACII, HEIGHT, V2TI, A.V)
1890 CALL CONFRACII, HEIGHT, Q2T1, A, Q)
1900 GO TO 199
1910 3 CALL CONFRACII, HEIGHT, V3TI, A, V)
1920 CALL CONFRACII, HEIGHT, Q3TI, A, Q)
1930 GO TO 199
1940 4 CALL CONFRACII, HEIGHT, V4T1, A, V)
1950 CALL CONFRACII, HEIGHT, Q4TI, A, Q)
1960 GO TO 199
1970 5 CALL CONFRACII, HEIGHT, VIT2, A, V)
1980 CALL CONFRACII, HEIGHT, QIT2, A, Q)
1990 CO TO 199
2000 6 CALL CONFRA(11, HEIGHT, V2T2, A, V)
2010 CALL CONFRACII, HEIGHT, Q2T2, A, Q)
2020 GO TO 199
2030 7 CALL CONFRACII, HEIGHT, V3T2, A, V)
2040 CALL CONFRACII, HEIGHT, Q3T2, A, Q)
2050 GO TO 199
2060 8 CALL CONFRAC11, HEIGHT, V4T2, A, V)
2070 CALL CONFRACII, HEIGHT, Q4T2, A, Q)
2080 GO TO 199
2090 9 V=0.
2100 CALL CONFRACII, HEIGHT, QIT3, A, Q)
2110 GO TO 199
2120 10 V=0.
2130 CALL CONFRACII, HEIGHT, Q2T3, A, Q)
2140 GO TO 199
2150 11 V=0.
2160 CALL CONFRACII, HEIGHT, Q3T3, A,Q)
2170 GO TO 199
2180 12 V=0.
2190 CALL CONFRACII, HEIGHT, Q4T3, A.Q)
2800 199 CONTINUE
2810 A = A - 1000.*DELP
2820 OTP = Q
2830 TC= 5./9.*(T-492.)
2840 S=(100./29.1)*OTP
2850 CALL CONFRA(10, VEL, PITCH, V, BETA)
2860 ALPHA = (BETA - TILT) +DTR
2870 VO=V*1.67
2880 HEL = HELOGW
2882 CALL CONFRA(5, AO, TO, A, T1)
2884 CALL CONFRA(5, AO, D1, A, D)
2886 CALL CONFRA(5, AO, LI, A, L)
2890 SIGMAE = CHORD*BLADES/(PI*RADIUS)
```

2892 SPDRTO = VO+COS(ALPHA)/(2.\*PI\*ROTSPD\*RADIUS)



```
14.27.43
                                    73/09/25
OHTURB -- PAGE 4
     PWREQ = PI**4*D*ROTSPD**3*RADIUS**5*DRAG
      PUREQ = PUREQ *SICMAE * (1.+SPDRTO * *2)
2896
      PWRAVL - PWREFF +550 . +5
2898
2900
      VIN = (PWRAUL - PWREQ) + COS(ALPHA)/HEL + VO+SIN(ALPHA)
2910 IF (VIN-LT-0.) VIN=-01
2920 CALL CONFRA(6,50, 11,5, 49(1))
2930 CALL CONFRA(6,50, 62,5, W9(2))
2940 CALL CONFRA(6, SO, W3, S, W9(3))
2950 CALL CONFRA(6,50, 44,5, 49(4))
2960 CALL CONFRA(4, SO, W5, S, W9(5))
2970 CALL CONFRA(6, SO, U1, S, U9(1))
2980 CALL CONFRA(6,50,U2,5,U9(2))
2990 CALL CONFRA(6, SO, U3, S, U9(3))
3000 CALL CONFRA(6,50,U4,S,U9(4))
3010 CALL CONFRA(4,50,U5,5,U9(5))
3020 CALL CONFRA(6,50,F1,5,F9)
3030 CALL CONFRA(5, AO, W9, A, W8)
3040 CALL CONFRA(5, A0, U9, A, U8)
3050 F8=F9
3090 D2=D*T1/T
3100 M1=T1/519
3110 M2=SQRT(M1)
3120 CALL CONFRA(9, T2, C1, T1, C4)
3130 CALL CONFRA(9, T2, C2, T1, C5)
3140 CALL CONFRA(9, T2, C3, T1, C6)
3150 CALL CONFRA(9, T2, C1, T, C7)
3160 CALL CONFRA(9, T2, C2, T, C8)
3170 CALL CONFRA(9, T2, C3, T, C9)
3180 R3=5/(L+M2)
3190 CALL CONFRA(6,R1,R2,R3,R4)
3200 R5=R4+T/519.
3810 W6 = W8*(1.+(C7-C4)/(1.+C4))
3220 U6 = U8*(1.+(C8-C5)/(1.+C5))
3230 F5=F8-(W8*V0)/G
3240 \text{ F6} = \text{F5+(L+C9-W8+(1++C7)+V0/G)-(L+C6-W8+(1++C4)+V0/G)}
3250 Q1=1.+U6/(W6+3600.)
3260 V7=(G*F6/W6+2.*V0)/Q1
3270 T7 = R5-V7**2/(2.*G*H*E)
3280 A7=(W6+T7+Q1)/(C+D2+T+V7)
3285 A7=A7/2.
3290 D7=24. *SQRT(A7/3.1416)
3300 PRINT 222, A, T, THROST, HELOGW
3305 222 FORMAT(//*ALTITUDE(FT) = *,F12.4/
3310+* AMBIENT TEMPERATURE (R) = *,F12.4/
3315+* THROTTLE SETTING = *,14/
3320+* GROSS WEIGHT (LBS) = *,110)
3330 PRINT 225, V, S, V7, T7, D7, Q1, BETA, VIN
3332 225 FORMAT(//* VELOCITY (KNOTS) IAS = *,F12.4/
3334+* SHP = *,F12.4/
3336+* EXIT VELOSITY (FT/SEC) = *,F12.4/
3338+* EXIT TEMPERATURE (R) = *,F12.4/
3340+* EXIT DIAMETER (INCHES) - *, F12-4/
3342++ 1 + FUEL/AIR RATIO = +,F12.4/
3344+* HELICOPTER PITCH (DEG) = *,F12.4/
3350+* DOWN WASH VELOSITY (FT/SEC) - *,F12.4)
```



```
OHTURB -- PAGE 5
                       14-27-43
                                    73/09/25
 3355 END
           PHILLIPS INTERPOLATION RUTINE
 03360*C
 03370*C
 03380*C
 03390 SUBROUTINE CONFRACN, X, Y, XI, YI)
 03400 DIMENSION X(1),Y(1)
 03410 IF(XI.LT.X(1))60 TO 100
 03420 IF(XI.GT.X(N))GO TO 110
 03430 DO 10 I=2.N
 03440 II=I
 03450 IF(XI.LT.X(I))GO TO 20
 03460 10 CONTINUE
 03470 20 12=11+1
 03480 11=11
03490 10=11-1
03500 NN=N+1
03510 IF(12.NE.NN)GO TO 40
03520 12=11
 03530 11=11-1
03540 ID=II-2
03550 40 A1=(XI-X(I1))*(XI-X(I2))/((X(I0)-X(I1))*(X(I0)-X(I2)))
03560 A2=(XI-X(10))*(X1-X(12))/((X(11)-X(10))*(X(11)-X(12)))
 03570 A3=(XI-X(10))*(XI-X(11))/((X(12)-X(10))*(X(12)-X(11)))
03580 YI=A1*Y(10)+A2*Y(11)+A3*Y(12)
03590 GO TO 1000
03600 100 12=1
03610 11=2
03620 10=3
03630 GO TO 120
03640 110 12=N
03650 I1=N-1
 03660 IO=N-2
03670 120 A=(X(10)-X(12))
03680 Y2P=(Y(12)-Y(11))/(X(12)-X(11))
03690 A=A*A
03700 B=(X(I1)-X(I2))
03710 B=B*B
03720 C=X(10)-X(11)
03730 DEN=A*B*C
03740 D1=(Y(10)-Y2P*(X(10)-X(12))-Y(12))*B
03750 D2=(Y(11)-Y2P*(X(11)-X(12))-Y(12))*A
03760 AA=(D1-D2)/DEN
03770 D1=D1+B
 03780 D2=D2*A
03790 BB=(D2-D1)/DEN
03800 A=XI-X(12)
03810 A=A*A*A
03820 B=XI-X(12)
 03830 B=B+B
03840 YI=AA*A+BB*B+Y2P*(XI-X(I2))+Y(I2)
03850 1000 GO TO 1500
03860*C TO PRINT OUT INTERPOLATIONS CHANGE STATMENT 1000 TO CONTINUE
03870 PRINT 1010, XI, YI
03880 PRINT 1020, (X(I), I=1,N)
03890 PRINT 1020, (Y(I), I=1,N)
```



OHTURB -- PAGE 6 14.27.43 73/09/25

03900 1010 FORMAT(//\*X=\*F10.4,\*Y=\*F10.4)
03910 1020 FORMAT(9F8.3)
03920 1500 CONTINUE
03930 RETURN
03940 END

LENGTH = 280 LINES



APPENDIX C (U)

SELECTED DATA

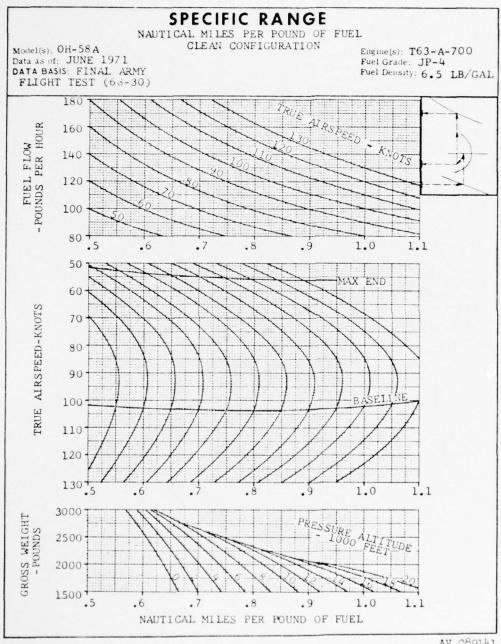
FROM THE

OH-58

OPERATOR'S MANUAL



TM 55-1520-228-10



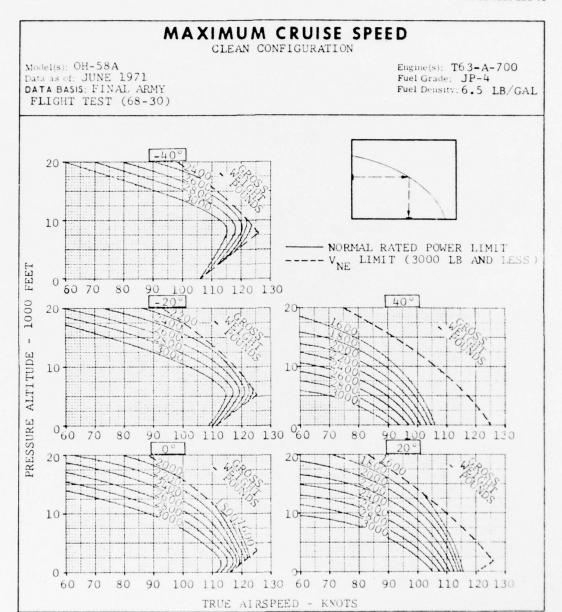
AV 089141

Specific range - clean

C-2



TM 55-1520-228-10



AV 089145

Maximum cruise speed - clear



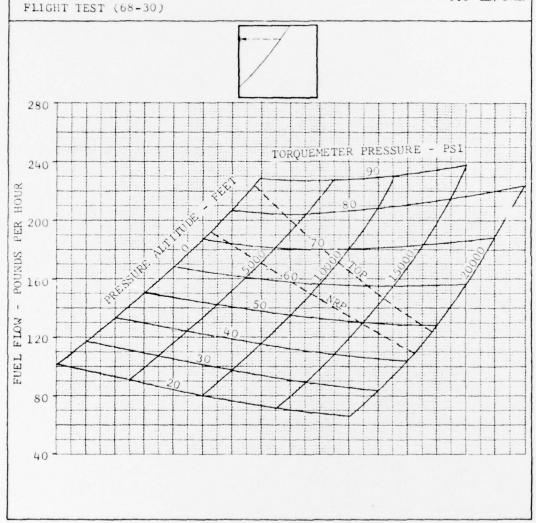
TM 55-1520-228-10

### **FUEL FLOW**

Model(s): OH-58A Data as of: JUNE 1971 DATA BASIS: FINAL ARMY

STANDARD DAY 6180 RPM WITH PARTICLE SEPARATOR

Engine(s): T63-A-700 Fuel Grade: JP-4 Fuel Density: 6.5 LB/GAL



AV 089124

Fuel flow chart

C-4



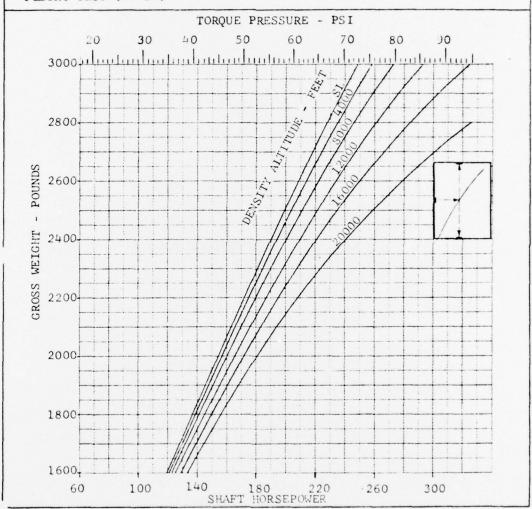
TM 55-1520-228-10

### TORQUE AND POWER REQUIRED TO HOVER

OUT OF GROUND EFFECT ALL CONFIGURATIONS

Model(s): OH-58A Data as of: JUNE 1971 DATA BASIS: FINAL ARMY FLIGHT TEST (68-30) Engine(s): T63-A-700 Fuel Grade: JP-4

Fuel Density: 6.5 LB/GAL



AV 089127

Torque and power required to hover OGE



APPENDIX D (U)

SELECTED DATA FROM

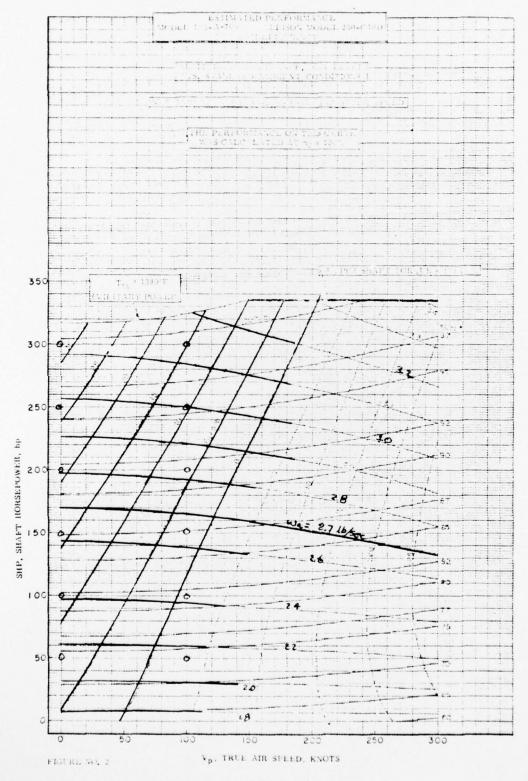
ALLISON

ON THE

TURBILE

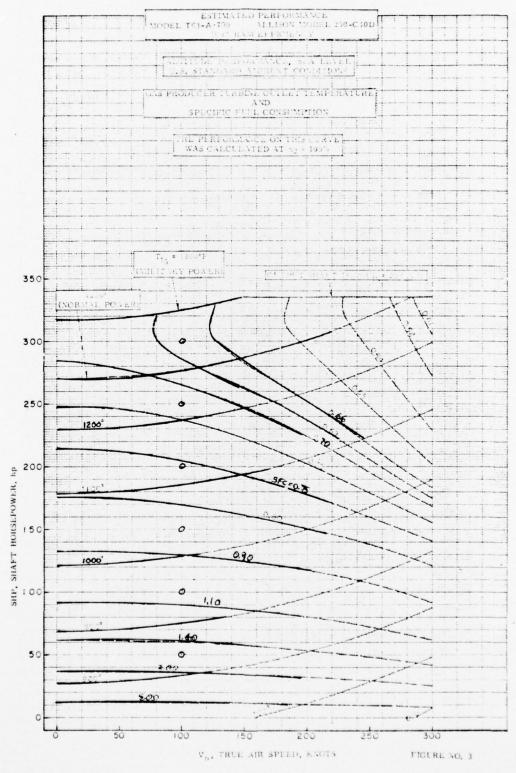
T63-A-700





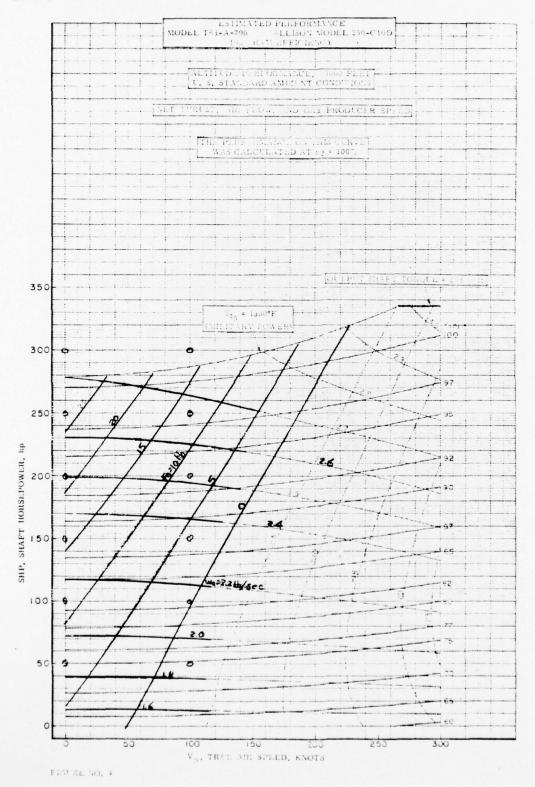
D-2



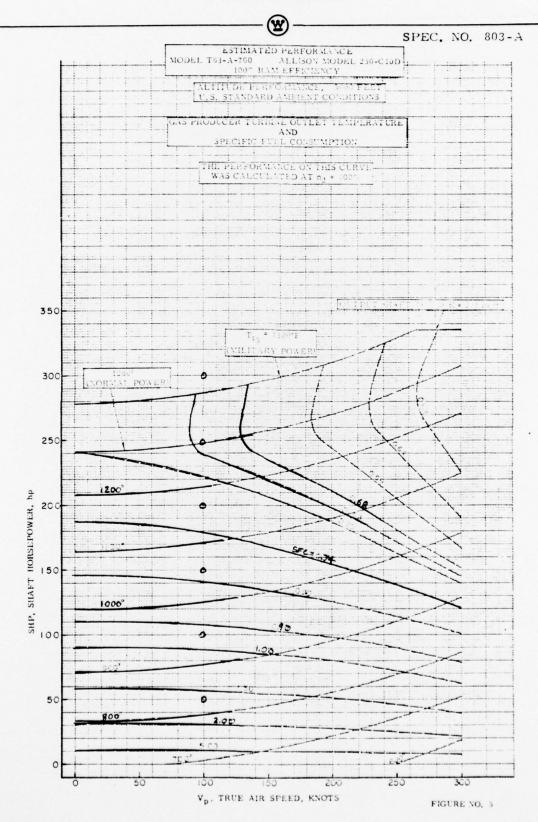


D-3



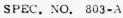


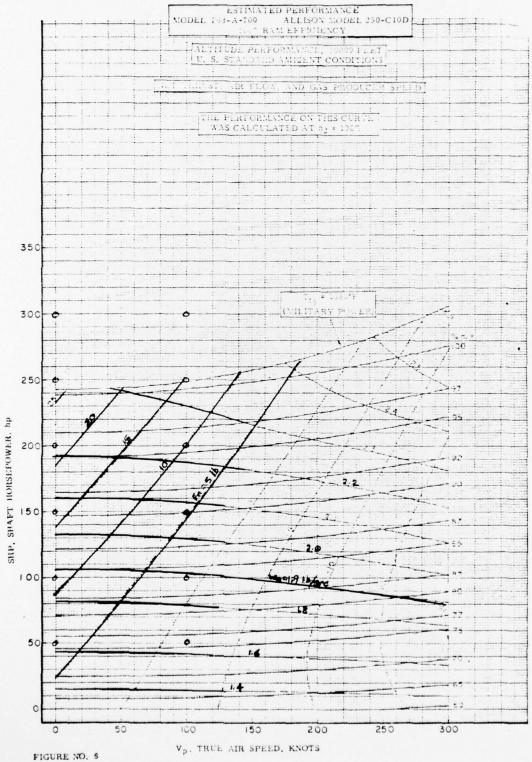
D-4



D-5

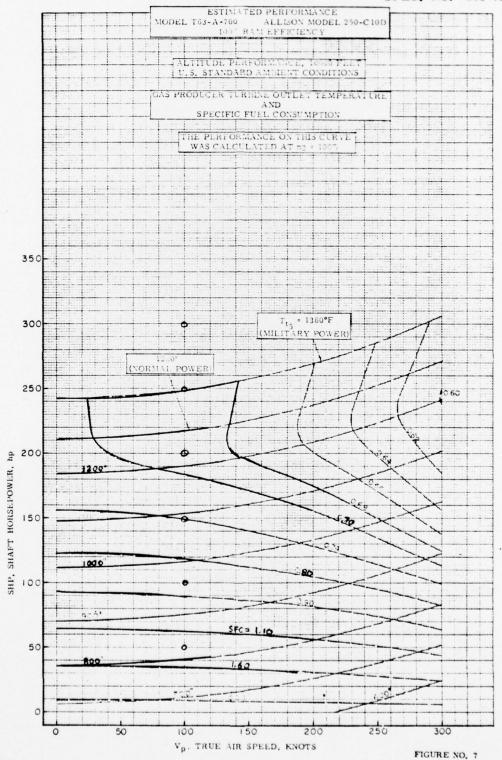






D-6







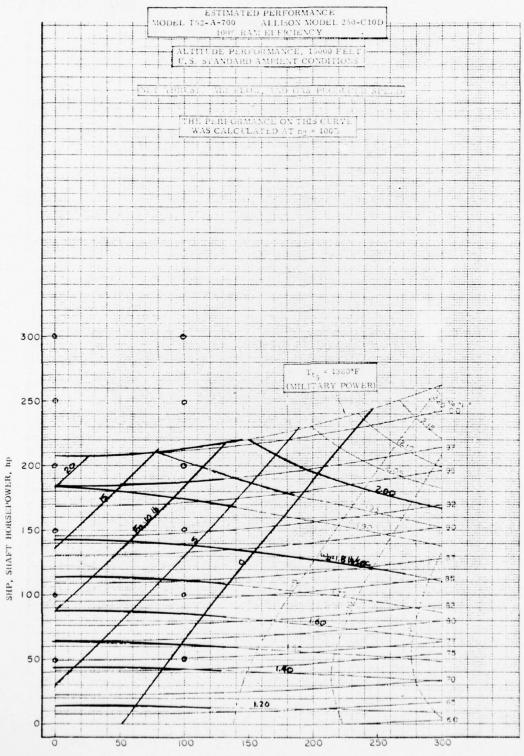


FIGURE NO. 8

 $v_p$ , TRUE AIR SPEED, KNOTS



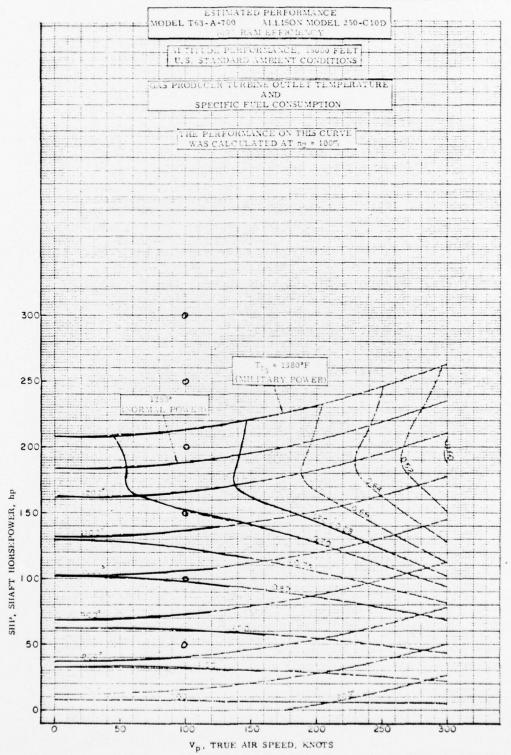
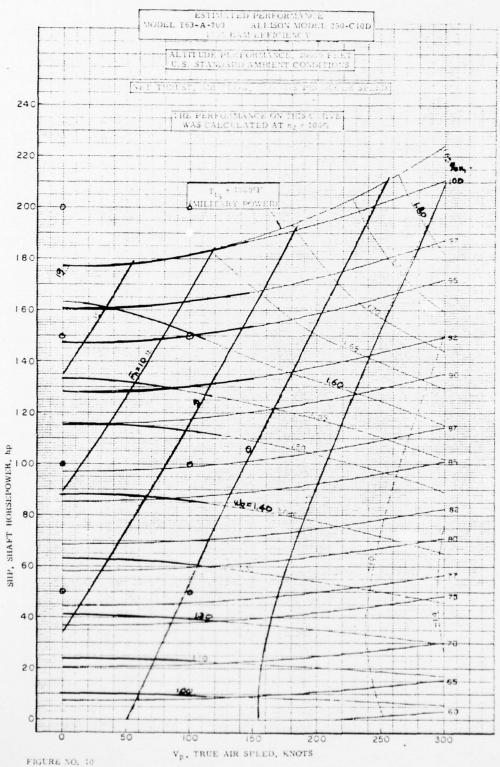
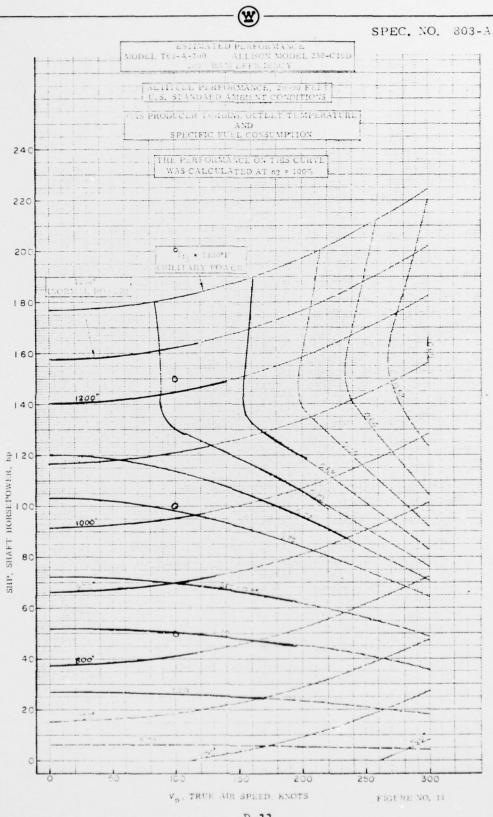


FIGURE NO. 9



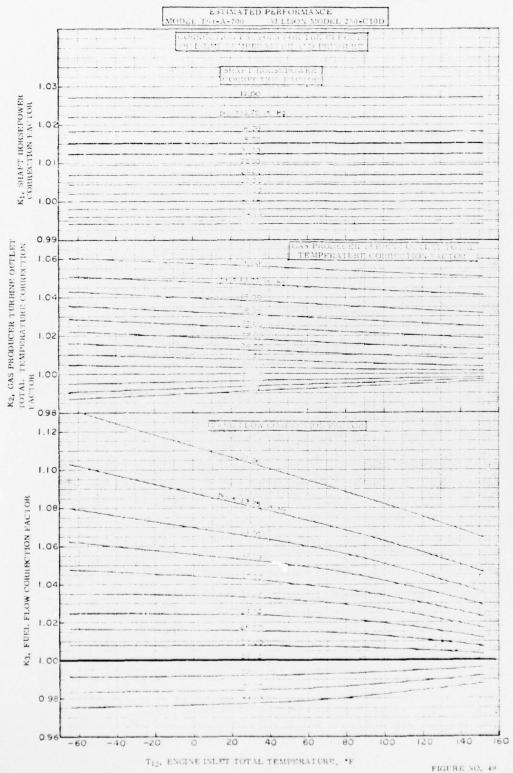


D-10



D-11





D-12